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ORIGINAL RESEARCH

Hemodynamic analysis of fast and slow aneurysm occlusions by flow diversion in rabbits

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ABSTRACT

Purpose To assess hemodynamic differences between aneurysms that occlude rapidly and those occluding in delayed fashion after flow diversion in rabbits.

Methods Thirty-six elastase-induced aneurysms in rabbits were treated with flow diverting devices.

Aneurysm occlusion was assessed angiographically immediately before they were sacrificed at 1 (n=6), 2 (n=4), 4 (n=8) or 8 weeks (n=18) after treatment. The aneurysms were classified into a fast occlusion group if they were completely or near completely occluded at 4 weeks or earlier and a slow occlusion group if they remained incompletely occluded at 8 weeks. The immediate post-treatment flow conditions in aneurysms of each group were quantified using subject-specific computational fluid dynamics and statistically compared.

Results Nine aneurysms were classified into the fast occlusion group and six into the slow occlusion group. Aneurysms in the fast occlusion group were on average significantly smaller (fast=0.9 cm, slow=1.393 cm, p=0.024) and had smaller ostia (fast=0.144 cm², slow=0.365 cm², p=0.015) than aneurysms in the slow occlusion group. They also had a lower mean post-treatment inflow rate (fast=0.047 mL/s, slow=0.155 mL/s, p=0.0239), kinetic energy (fast=0.519 erg, slow=1.283 erg, p=0.0468), and velocity (fast=0.221 cm/s, slow=0.506 cm/s, p=0.0582). However, the differences in the latter two variables were only marginally significant.

Conclusions Hemodynamic conditions after flow diversion treatment of cerebral aneurysms in rabbits are associated with the subsequent aneurysm occlusion time. Specifically, smaller inflow rate, kinetic energy, and velocity seem to promote faster occlusions, especially in smaller and small-necked aneurysms. These results are consistent with previous studies based on clinical series.

INTRODUCTION

Flow diversion is increasingly being used to treat wide-necked intracranial aneurysms that are difficult to treat with coils alone.^{1–3} However, flow diversion does not immediately exclude the aneurysm from the circulation. Therefore, until the aneurysm thromboses and occludes, it remains exposed to mechanical loads and biological processes that could potentially cause its rupture.⁴ Presumably, reducing the time it takes to completely occlude an aneurysm could prevent complications such as delayed ruptures.^{4,5} Predicting or controlling the occlusion time after flow diversion is therefore important to improve the outcomes of these procedures and avoid complications. The purpose of this study was to assess the differences

in the hemodynamic environment generated immediately after placement of flow diverting devices between aneurysms that occluded quickly and those that remained patent in a series of experimentally created aneurysms in rabbits.

METHODS

Animal models

A total of 36 elastase-induced aneurysms were created in New Zealand white rabbits following the approach described by Altes *et al.*⁶ Four weeks after their creation the aneurysms were imaged with 3D rotational angiography (3DRA) and flow velocities in the surrounding vessels were measured with Doppler ultrasound. Subsequently, the aneurysms were treated with a flow diverting device (Pipeline Embolization Device, Covidien). Two days before embolization the animals were premedicated with aspirin (10 mg/kg orally) and clopidogrel (10 mg/kg orally). This medication regime was continued for 1 month after embolization. Some of the rabbits employed in this work were used as part of other studies^{7,8} entirely unrelated to the current study. This animal research was conducted with appropriate institutional approvals.

Angiographic evaluation

The animals were sacrificed within 1 week (n=6), at 2 weeks (n=4), at 4 weeks (n=8), and at 8 weeks (n=18) after treatment. Immediately before they were sacrificed, angiographic imaging including 3DRA was repeated and the degree of aneurysm occlusion was categorized as: (1) complete occlusion (no remnant); (2) near complete occlusion (small remnant); or (3) incomplete occlusion (substantial filling of the aneurysm).

Hemodynamic modeling

Computational fluid dynamics (CFD) models of the aneurysms were constructed using subject-specific vascular geometries derived from the pretreatment 3DRA images and pulsatile flow conditions from the Doppler ultrasound measurements.⁷ Models of the implanted flow diverting devices were created and virtually deployed into the vascular models.⁹ Vessel walls were assumed rigid, blood density was set to $\rho=1.0$ g/cm³, and the Newtonian blood viscosity to $\mu=0.04$ Poise. The unsteady incompressible Navier–Stokes equations were numerically solved using finite elements and adaptive immersed unstructured grids.¹⁰



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Data analysis

Aneurysms were classified into two groups according to the end time (time to sacrifice after treatment) and the degree of occlusion. Group 1, the 'fast occlusion' group, included aneurysms that were completely or near completely occluded within 1 week, at 2 weeks or at 4 weeks. Group 2, the 'slow occlusion' group, included aneurysms that were incompletely occluded at 8 weeks. In order to keep the fast and slow occlusion groups well defined and with no overlap, subjects not within these two groups were excluded from further analysis. The geometry and post-treatment hemodynamics of each aneurysm were characterized by computing a number of variables from the 3D CFD models. All variables considered were averaged over the aneurysm region and over the cardiac cycle. Exact definitions of the variables can be found in previous reports.^{8 11 12} The geometric and hemodynamic variables computed over the slow and fast occlusion groups were then statistically compared using the non-parametric Wilcoxon rank-sum test. Differences were considered significant if the p values were <0.05 (95% confidence). All statistical analyses were performed using SAS V.9.4 (Cary, North Carolina, USA).

Table 1 End point, occlusion status and grouping of aneurysms

Case	End time (weeks)	Occlusion	Group
1	<1	Incomplete	–
2	<1	Incomplete	–
3	<1	Incomplete	–
4	<1	Near complete	Fast
5	<1	Near complete	Fast
6	<1	Complete	Fast
7	2	Incomplete	–
8	2	Near complete	Fast
9	2	Incomplete	–
10	2	Incomplete	–
11	4	Near complete	Fast
12	4	Near complete	Fast
13	4	Incomplete	–
14	4	Complete	Fast
15	4	Incomplete	–
16	4	Incomplete	–
17	4	Near complete	Fast
18	4	Near complete	Fast
19	8	Incomplete	Slow
20	8	Incomplete	Slow
21	8	Incomplete	Slow
22	8	Incomplete	Slow
23	8	Incomplete	Slow
24	8	Incomplete	Slow
25	8	Near complete	–
26	8	Near complete	–
27	8	Near complete	–
28	8	Near complete	–
29	8	Near complete	–
30	8	Complete	–
31	8	Complete	–
32	8	Complete	–
33	8	Complete	–
34	8	Complete	–
35	8	Complete	–
36	8	Complete	–

RESULTS

The end time, degree of occlusion, and corresponding occlusion group of each aneurysm are presented in [table 1](#). A total of six aneurysms were classified into the slow occlusion group and nine into the fast occlusion group. The mean and SD of geometric and hemodynamic variables computed over these two groups are shown in [table 2](#) along with the corresponding p values.

Ratios of mean geometric and hemodynamic variables of the slow over the fast occlusion groups are graphically presented in [figure 1](#). Bars above 1 indicate that the mean value of the slow occlusion group is larger than the mean value of the fast occlusion group.

Aneurysms in the fast occlusion group had significantly lower mean size (fast=0.900 cm, slow=1.393 cm, p=0.024), volume (fast=0.205 cm³, slow=0.723 cm³, p=0.030), area (fast=0.982 cm², slow=1.806 cm², p=0.038), and neck area (fast=0.144 cm, slow=0.365 cm², p=0.015) than aneurysms in the slow occlusion group. They also had lower mean post-treatment inflow rate (fast=0.047 mL/s, slow=0.155 mL/s, p=0.0239), kinetic energy (fast=0.519 erg, slow=1.283 erg, p=0.0468), and velocity (fast=0.221 cm/s, slow=0.506 cm/s, p=0.0582). However, the differences of the latter two variables were only marginally significant. The inflow concentration, shear rate, vorticity, viscous dissipation, and wall shear stress (WSS) tended to be larger in the slow occlusion group but there was no statistical significance (p>0.05). The maximum and minimum WSS, oscillatory shear index, area under low WSS, flow complexity (CORELEN) and stability (PODENT), and mean aneurysm

Table 2 Summary statistics of geometric and hemodynamic variables in the slow and fast occlusion groups

Variable	Slow occlusion		Fast occlusion		p Value
	Mean	SD	Mean	SD	
Aneurysm volume (VOL)	0.723	0.495	0.205	0.238	0.0299
Maximum diameter (SIZE)	1.393	0.294	0.900	0.235	0.0239
Aneurysm area (AREA)	1.806	0.678	0.982	0.372	0.0375
Neck area (NECK)	0.365	0.082	0.144	0.078	0.0151
Maximum distance to neck (DEPTH)	0.920	0.255	0.687	0.197	0.0891
Aspect ratio (AR)	1.238	0.375	1.539	0.427	0.3917
Inflow concentration index (ICI)	0.013	0.035	0.007	0.010	0.2817
Aneurysm inflow rate (Q)	0.155	0.095	0.047	0.053	0.0239
Kinetic energy (KE)	1.283	1.010	0.519	0.967	0.0468
Shear rate (SR)	7.160	3.326	4.009	3.514	0.0722
Velocity (VE)	0.506	0.298	0.221	0.241	0.0582
Vorticity (VO)	7.714	4.220	4.294	4.221	0.0891
Viscous dissipation (VD)	2.807	1.664	1.650	2.353	0.1968
Maximum WSS (WSSmax)	92.635	95.690	63.854	32.524	0.7726
Minimum WSS (WSSmin)	0.000	0.000	0.000	0.000	0.6862
Mean WSS (<WSS>)	0.684	0.233	0.407	0.275	0.0891
Low WSS area (LSA)	59.908	28.391	69.925	29.239	0.5274
WSS concentration index (SCI)	10.888	15.718	11.549	9.296	0.3917
Maximum oscillatory shear index (OSImax)	0.489	0.008	0.484	0.031	0.6042
Mean oscillatory shear index (<OSI>)	0.319	0.119	0.371	0.109	0.2817
Vortex coreline length (CORELEN)	1.352	0.562	1.127	0.469	0.6862
Entropy of POD modes (PODENT)	0.720	0.250	0.588	0.206	0.3335
Mean aneurysm transit time (MATT)	6.222	4.441	14.060	15.209	0.5274

POD, proper orthogonal decomposition; WSS, wall shear stress.

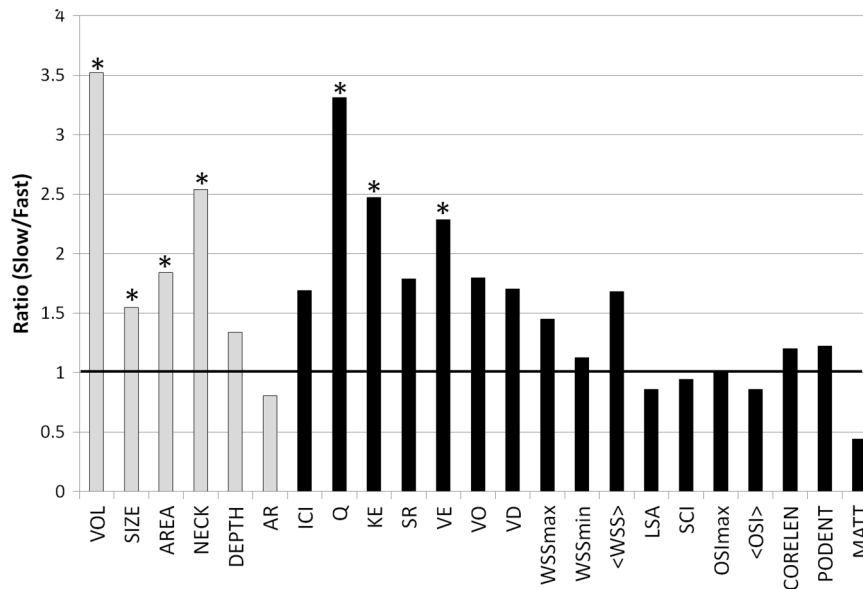


Figure 1 Ratio of average geometric (gray bars) and hemodynamic (black bars) variables of the slow over the fast occlusion groups. Bars above 1 indicate that the mean value of the slow occlusion group is larger than the mean value of the fast occlusion group. Statistically significant differences between the two groups are marked with an asterisk. For definitions of abbreviations, see table 1.

transit time as well as the aspect ratio and aneurysm depth were not statistically different between the two groups ($p > 0.05$).

Flow visualizations of three example aneurysms are presented in figure 2. From top to bottom, this figure shows isovelocity ($v = 10$ cm/s) before and after treatment and velocity streamlines before and after treatment. The first aneurysm (left column) was completely occluded before 1 week (fast occlusion), the second aneurysm (center column) was completely occluded at 4 weeks (fast occlusion), and the third aneurysm was incompletely occluded at 8 weeks (slow occlusion). It can be seen that, immediately after treatment, the inflow stream into aneurysms 1 and 2 is substantially reduced while in aneurysm 3 there is still a notable inflow into the aneurysm. The flow pattern in aneurysm 1 changed significantly after treatment. In particular, the inflow shifted to the proximal end of the neck and the intrasaccular streamlines followed a simpler and smoother trajectory. Aneurysm 2 follows the same general trend but with a slightly larger flow activity within the aneurysm sac. The flow structure in aneurysm 3 did not change markedly, although the blood speed along the streamlines was reduced.

DISCUSSION

Currently there is no reliable technique to evaluate flow diversion treatments of intracranial aneurysms and to predict their long-term outcomes. Previous studies have focused on the identification of qualitative and/or quantitative characteristics that could be used to prognosticate the outcomes of flow diversion therapies.^{13–18} However, the effects of flow diverting devices and the underlying mechanisms governing the thrombosis and occlusion of cerebral aneurysms are still not well understood.

Our current study used rabbit models to demonstrate that the flow conditions created immediately after placement of flow diverting devices are quantitatively different between aneurysms that subsequently occluded quickly and those that remained patent for a longer period of time. In particular, the flow diverters more efficiently blocked the inflow stream and the resulting mean aneurysm velocity and flow activity were significantly smaller in fast occluding aneurysms. In the present study, no balloons were used to expand the devices and all devices were

reasonably well appositioned against the parent artery wall covering the entire aneurysm orifice, except for two aneurysms of the slow occlusion group. In these two cases, the proximal end of the devices were not completely apposed to the wall which allowed a thin flow stream to slide between the device and the wall and to enter the aneurysm (see aneurysm 3 in figure 2). Imperfect deployments can have a substantial impact on the occlusion time and outcome of flow diverting procedures.

Our results are consistent with previous studies based on clinical series.^{19,20} This adds support to the validity of the rabbit aneurysm models and also confirms the idea that post-treatment flow conditions could potentially be used to assess the technical success of flow diverting procedures and to predict the occlusion times and long-term outcomes. In particular, our study indicates that the mean aneurysm velocity, which can potentially be measured with dynamic angiography,²⁰ is a good predictor of occlusion time after flow diversion treatment. However, in clinical situations there may be other factors besides hemodynamics and morphology that could affect the occlusion time after flow diversion, including response to antiplatelet medication, comorbidities such as diabetes which are known to alter the vascular response to implants, and habits such as smoking which alter platelet function and tissue repair.

This study suffers from a number of limitations associated with assumptions and approximations made in the CFD modeling, such as rigid walls, Newtonian rheology, and idealized inflow profiles, as well as limitations of the rabbit models, such as flow reversal in the parent artery which does not occur in human cerebral arteries, and limited serial imaging that prevents visualization of the progression of aneurysmal occlusion. Nevertheless, these models allowed us to quantitatively compare the subject-specific hemodynamics between fast and slow aneurysm occlusion groups, and to identify target flow characteristics that could be used to accelerate the healing process after flow diversion and ultimately improve outcomes. These findings need to be further investigated and confirmed with larger series.

CONCLUSIONS

Hemodynamic conditions experimentally created immediately after flow diversion treatment of cerebral aneurysms in rabbits are

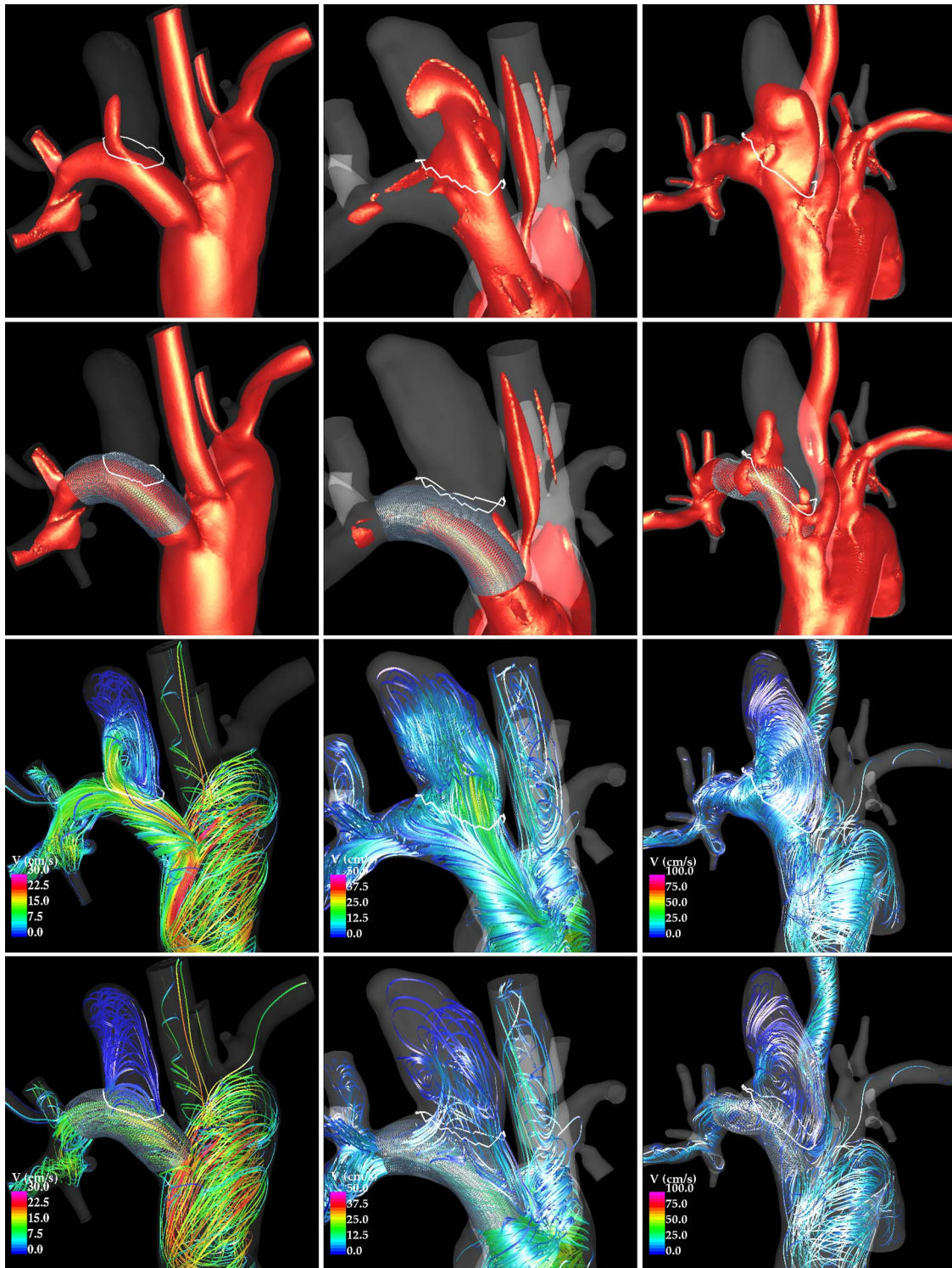


Figure 2 Flow visualizations in aneurysms occluded at 1 week (left column) and 4 weeks (center column), and in an aneurysm incompletely occluded at 8 weeks (right column). Each column shows, from top to bottom: isovelocity before treatment, isovelocity after treatment, flow streamlines before treatment, and flow streamlines after treatment.

associated with the subsequent aneurysm occlusion time. Specifically, smaller inflow rate, kinetic energy, and intrasaccular velocity seem to promote faster occlusions. These results are consistent with previous studies based on clinical series and could be used to prognosticate the long-term outcomes of flow diversion therapies.

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Contributors BC and FM performed CFD simulations and edited the manuscript. RK performed the animal experiments, collected data, and edited the manuscript. RL performed the statistical analysis. DFK and JRC conceived the work, analyzed and interpreted the results, and drafted the manuscript.

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Competing interests None.

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